

Ch4: Rigid-Body Motion – Transformation

Transformation Matrices

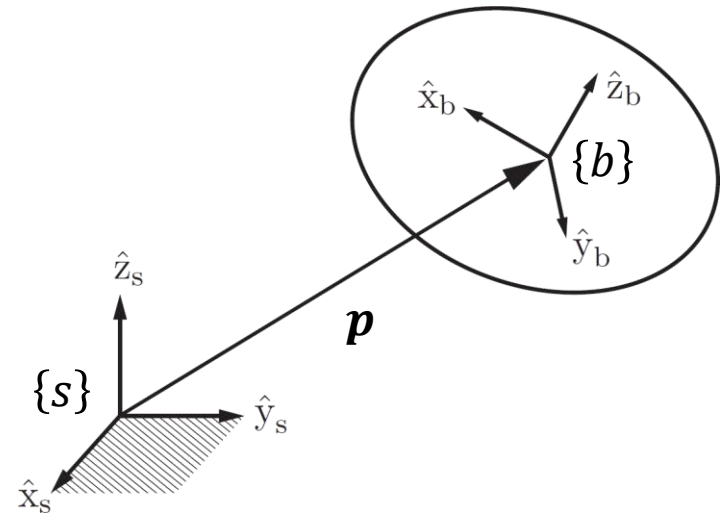
Homogeneous Transformation Matrices

Rigid-body configuration can be represented by the pair (\mathbf{R}, \mathbf{p}) ($\mathbf{R} \in SO(3)$, $\mathbf{p} \in \mathbb{R}^3$). We can package (\mathbf{R}, \mathbf{p}) into a single 4×4 matrix as

$$\mathbf{T} = \begin{bmatrix} \mathbf{R} & \mathbf{p} \\ \mathbf{0} & 1 \end{bmatrix}$$

Transformation Matrix

This is as Implicit representation the C-space.



$$\mathbf{R} := \mathbf{R}_{sb}$$

$$\mathbf{p} := \mathbf{p}_s = \mathbf{p}_s^b = \mathbf{p}_s^{sb}$$

Special Euclidean Group $SE(n)$

The **Special Euclidean Group** $SE(3)$, also known as the **group of rigid-body motions** or **homogeneous transformation matrices** in \mathbb{R}^3 , is the set of all 4×4 real matrices \mathbf{T} of the form

$$\mathbf{T} = \begin{bmatrix} \mathbf{R} & \mathbf{p} \\ \mathbf{0} & 1 \end{bmatrix} = \begin{bmatrix} r_{11} & r_{12} & r_{13} & p_1 \\ r_{21} & r_{22} & r_{23} & p_2 \\ r_{31} & r_{32} & r_{33} & p_3 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad \begin{array}{l} \mathbf{T} \in SE(3) \\ \mathbf{R} \in SO(3) \\ \mathbf{p} \in \mathbb{R}^3 \end{array}$$

$$SE(3) = \left\{ \mathbf{T} \in \mathbb{R}^{4 \times 4} \mid \mathbf{T} = \begin{bmatrix} \mathbf{R} & \mathbf{p} \\ \mathbf{0} & 1 \end{bmatrix}, \mathbf{R} \in SO(3), \mathbf{p} \in \mathbb{R}^3 \right\}$$

The **special Euclidean group** $SE(2)$ is the set of all 3×3 real matrices \mathbf{T} of the form

$$\mathbf{T} = \begin{bmatrix} \mathbf{R} & \mathbf{p} \\ \mathbf{0} & 1 \end{bmatrix} = \begin{bmatrix} r_{11} & r_{12} & p_1 \\ r_{21} & r_{22} & p_2 \\ 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} \cos \theta & -\sin \theta & p_1 \\ \sin \theta & \cos \theta & p_2 \\ 0 & 0 & 1 \end{bmatrix} \quad \begin{array}{l} \mathbf{T} \in SE(2) \\ \mathbf{R} \in SO(2) \\ \mathbf{p} \in \mathbb{R}^2 \\ \theta \in [0, 2\pi) \end{array}$$

- $SE(2)$ is a subgroup of $SE(3)$: $SE(2) \subset SE(3)$

Properties of Transformation Matrices

$SE(3)$ (or $SE(2)$) is a **matrix (Lie) group** (and the group operation \bullet is matrix multiplication).

Closure: $T_1 T_2 \in SE(3)$

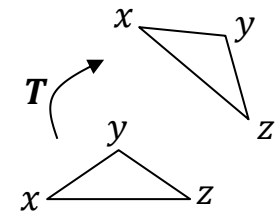
Associative: $(T_1 T_2) T_3 = T_1 (T_2 T_3)$ (but generally not commutative, $T_1 T_2 \neq T_2 T_1$)

Identity: $\exists I_4 \in SE(3)$ such that $T I_4 = I_4 T = T$

Inverse: $\exists T^{-1} \in SE(3)$ such that $T T^{-1} = T^{-1} T = I_4$

$$T^{-1} = \begin{bmatrix} \mathbf{R} & \mathbf{p} \\ \mathbf{0} & 1 \end{bmatrix}^{-1} = \begin{bmatrix} \mathbf{R}^T & -\mathbf{R}^T \mathbf{p} \\ \mathbf{0} & 1 \end{bmatrix}$$

Note: T preserves both distances and angles.

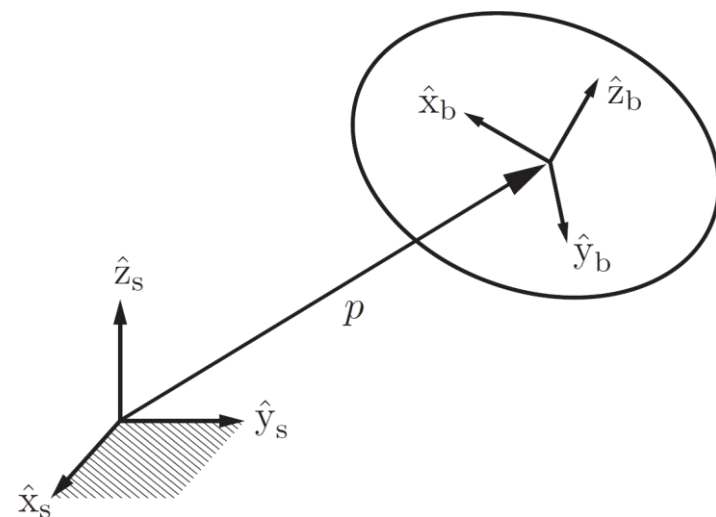


Uses of Transformation Matrices (1)

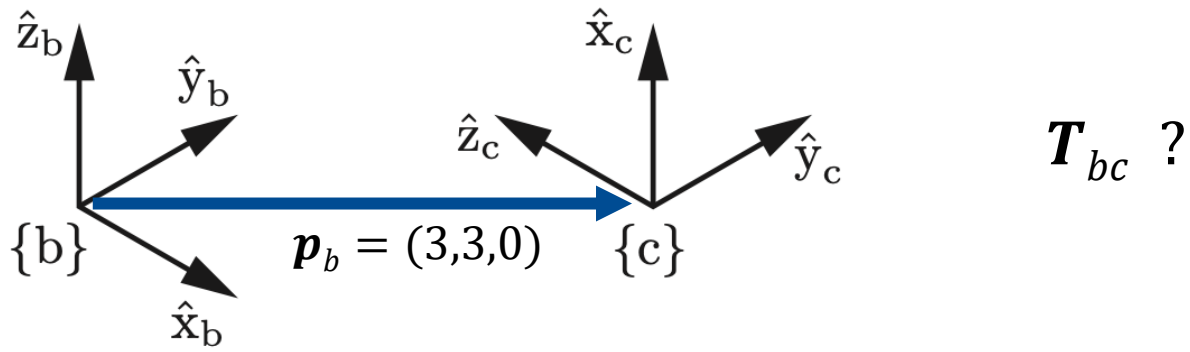
(1) Representing configuration (position and orientation) of a frame relative to another frame.

Notation: T_{sb} is the configuration of $\{b\}$ relative to $\{s\}$.

$$T_{sb} = \begin{bmatrix} R_{sb} & \mathbf{p} \\ \mathbf{0} & 1 \end{bmatrix}$$



Example



Uses of Transformation Matrices (2)

(2) Changing the reference frame of a vector or frame.

Subscript Cancellation Rule:

$$\mathbf{T}_{ab} \mathbf{v}_b = \mathbf{T}_{a\cancel{b}} \mathbf{v}_{\cancel{b}} = \mathbf{v}_a$$

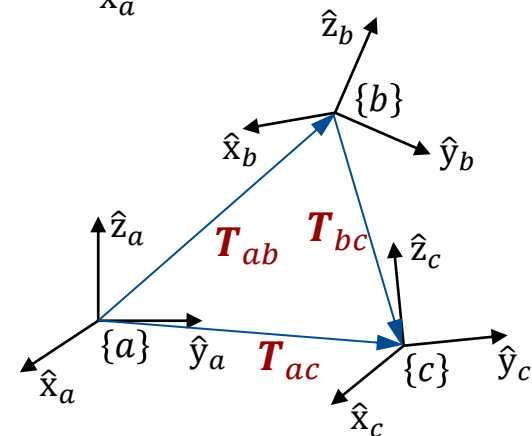
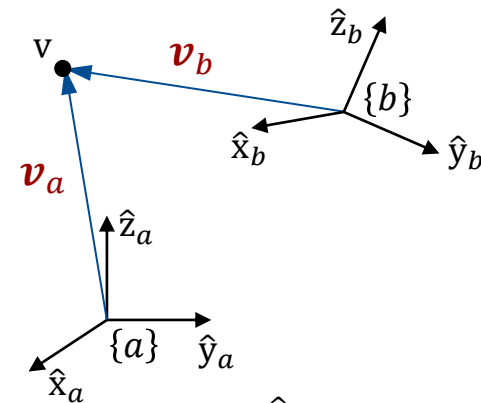
$$\mathbf{T}_{ab} \mathbf{T}_{bc} = \mathbf{T}_{a\cancel{b}} \mathbf{T}_{\cancel{b}c} = \mathbf{T}_{ac}$$

\mathbf{T}_{ab} can be viewed as a mathematical operator that changes the reference frame from $\{b\}$ to $\{a\}$.

Note: $\mathbf{T}_{bc} \mathbf{T}_{cb} = \mathbf{I}_4$ or $\mathbf{T}_{bc} = \mathbf{T}_{cb}^{-1} = \begin{bmatrix} \mathbf{R}_{cb}^T & -\mathbf{R}_{cb}^T \mathbf{p}_c^{cb} \\ \mathbf{0} & 1 \end{bmatrix}$

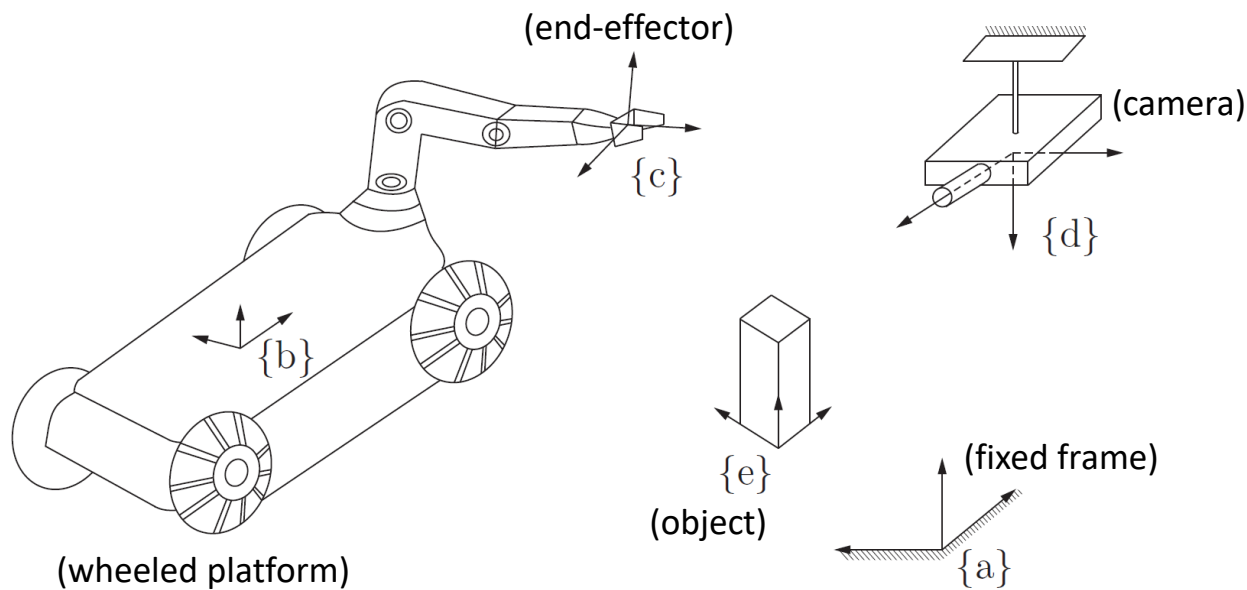
Note: To calculate $\mathbf{T}\mathbf{v}$, we append a "1" to \mathbf{v} and it is called **homogeneous coordinates** representation of \mathbf{v} .

$$\mathbf{v} = [v_1 \ v_2 \ v_3 \ 1]^T$$



Example

A robot arm mounted on a wheeled mobile platform moving in a room, and a camera fixed to the ceiling. The robot must pick up an object with body frame $\{e\}$. What is the configuration of the object relative to the robot hand, T_{ce} , given T_{db} , T_{de} , T_{bc} , and T_{ad} ?



Uses of Transformation Matrices (3)

(3) Displacing (rotating and translating) a vector or frame.

$$\mathbf{T} = (\mathbf{R}, \mathbf{p}) = (\text{Rot}(\hat{\boldsymbol{\omega}}, \theta), \mathbf{p}) = \text{Trans}(\mathbf{p})\text{Rot}(\hat{\boldsymbol{\omega}}, \theta)$$



$$\text{Rot}(\hat{\boldsymbol{\omega}}, \theta) = \begin{bmatrix} \mathbf{R} & \mathbf{0} \\ \mathbf{0} & 1 \end{bmatrix}$$

$$\text{Trans}(\mathbf{p}) = \begin{bmatrix} \mathbf{I}_3 & \mathbf{p} \\ \mathbf{0} & 1 \end{bmatrix}$$

\mathbf{T} can be viewed as a mathematical operator that rotates a frame or vector about a unit axis $\hat{\boldsymbol{\omega}} = (\hat{\omega}_1, \hat{\omega}_2, \hat{\omega}_3)$ by an amount θ + translating it by \mathbf{p} .

Uses of Transformation Matrices (3) (cont.)

- Rotation of vector \mathbf{v} about a unit axis $\hat{\omega}$ (expressed in the same frame) by an amount θ and translation of it by \mathbf{p} (expressed in the same frame) is vector \mathbf{v}' expressed in the same frame:

$$\mathbf{v}'' = \mathbf{T}\mathbf{v} = \text{Trans}(\mathbf{p})\text{Rot}(\hat{\omega}, \theta)\mathbf{v} \equiv \text{Rot}(\hat{\omega}, \theta)\mathbf{v} + \mathbf{p}$$

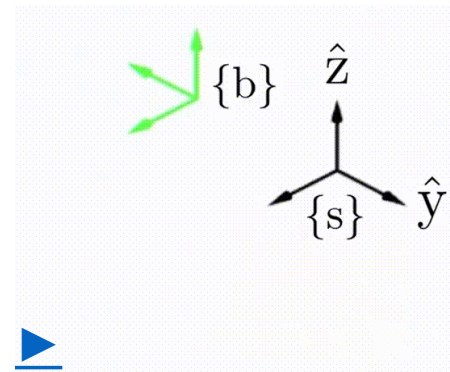
← Interpretation

Fixed-frame Transformation:

- Rotating $\{b\}$ by θ about $\hat{\omega}$ in $\{s\}$ (this can move $\{b\}$ origin) to get $\{b'\}$
- Translating $\{b'\}$ by \mathbf{p} in $\{s\}$ to get $\{b''\}$

$$\mathbf{T}_{sb''} = \mathbf{T}\mathbf{T}_{sb} = \text{Trans}(\mathbf{p})\text{Rot}(\hat{\omega}, \theta)\mathbf{T}_{sb}$$

(pre-multiplication) ← Interpretation

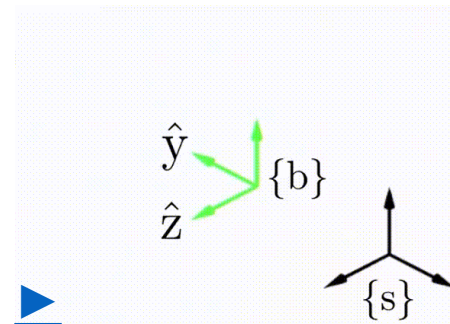


Body-frame Transformation:

- Translating $\{b\}$ by \mathbf{p} in $\{b\}$ to get $\{b'\}$
- Rotating $\{b'\}$ by θ about $\hat{\omega}$ in $\{b'\}$ to get $\{b''\}$

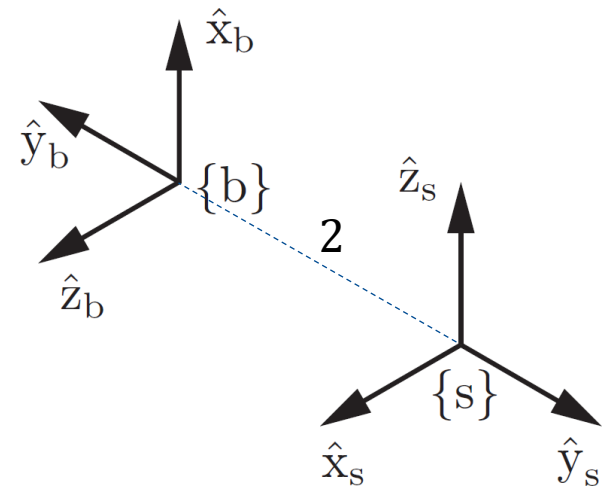
$$\mathbf{T}_{sb''} = \mathbf{T}_{sb}\mathbf{T} = \mathbf{T}_{sb}\text{Trans}(\mathbf{p})\text{Rot}(\hat{\omega}, \theta)$$

(post-multiplication) ← Interpretation



Example

Find fixed-frame and body-frame transformations corresponding to $\hat{\omega} = (0,0,1)$, $\theta = 90^\circ$, and $\mathbf{p} = (0,2,0)$.



Twist

Lie Algebra $se(3)$

- The set of all 4×4 matrices of the form

$$\begin{bmatrix} [\boldsymbol{\omega}] & \boldsymbol{v} \\ \mathbf{0} & 0 \end{bmatrix}$$

where $[\boldsymbol{\omega}] \in so(3)$ and $\boldsymbol{v} \in \mathbb{R}^3$ is called $se(3)$.

- $se(3)$ is the matrix representation of 6×1 vectors $\boldsymbol{\nu} = \begin{bmatrix} \boldsymbol{\omega} \\ \boldsymbol{v} \end{bmatrix} \in \mathbb{R}^6$. Thus,

$$[\boldsymbol{\nu}] = \begin{bmatrix} [\boldsymbol{\omega}] & \boldsymbol{v} \\ \mathbf{0} & 0 \end{bmatrix} \in se(3)$$

- $se(3)$ is called the Lie algebra of the Lie group $SE(3)$.

Spatial Velocity or Twist

A rigid body's **Spatial Velocity** or **Twist** can be represented as a point in \mathbb{R}^6 and defined as

$$\mathbf{v}_x = \begin{bmatrix} \text{angular velocity of body expressed in frame } \{x\} \\ \text{linear velocity of origin of frame } \{x\} \text{ on body (or its extention) expressed in frame } \{x\} \end{bmatrix} \in \mathbb{R}^6$$

expressed in $\{x\}$

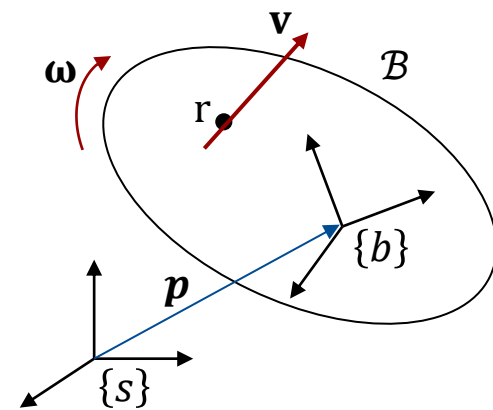
A general form:

$$\mathbf{v}_x^{B_r} = \begin{bmatrix} \text{angular velocity of body } \mathcal{B} \text{ expressed in frame } \{x\} \\ \text{linear velocity of point } r \text{ on body } \mathcal{B} \text{ (or its extention) expressed in frame } \{x\} \end{bmatrix} \in \mathbb{R}^6$$

point where velocity is computed
expressed in $\{x\}$

Let's find the twist $\mathcal{V} \in \mathbb{R}^6$ of a moving body (or body frame $\{b\}$) in terms of $\mathbf{T}_{sb} = \mathbf{T}(t)$. Body Frame $\{b\}$ is instantaneously coincident with the body-attached frame.

$$\mathbf{T}(t) = \begin{bmatrix} \mathbf{R}(t) & \mathbf{p}(t) \\ \mathbf{0} & 1 \end{bmatrix}$$



Body Twist \mathcal{V}_b

Similar to $R^{-1}\dot{R} = [\omega_b]$, let's compute $T^{-1}\dot{T}$: $(R := R_{sb}, T := T_{sb})$

$$\begin{aligned}
 T^{-1}\dot{T} &= \begin{bmatrix} R^T & -R^T p \\ \mathbf{0} & 1 \end{bmatrix} \begin{bmatrix} \dot{R} & \dot{p} \\ \mathbf{0} & 0 \end{bmatrix} \\
 &= \begin{bmatrix} R^T \dot{R} & R^T \dot{p} \\ \mathbf{0} & 0 \end{bmatrix} \\
 &= \begin{bmatrix} [\omega_b] & v_b \\ \mathbf{0} & 0 \end{bmatrix} \xrightarrow{[\omega_b] \in so(3)} T^{-1}\dot{T} = [\mathcal{V}_b] = \begin{bmatrix} [\omega_b] & v_b \\ \mathbf{0} & 0 \end{bmatrix} \in se(3)
 \end{aligned}$$

$$\mathcal{V}_b = \begin{bmatrix} \omega_b \\ v_b \end{bmatrix} \in \mathbb{R}^6 \quad \mathcal{V}_b \text{ is defined as } \mathbf{Body Twist} \text{ (or spatial velocity in the body frame)}$$

- $[\mathcal{V}_b] \in se(3)$ is the matrix representations of the **body twists** $\mathcal{V}_b \in \mathbb{R}^6$ associated with the rigid-body configuration $T \in SE(3)$.
- \mathcal{V}_b does not depend on the choice of the fixed frame $\{s\}$,

Spatial Twist \mathcal{V}_s

Similar to $\dot{R}R^{-1} = [\omega_s]$, let's compute $\dot{T}T^{-1}$: $(R = R_{sb}, T = T_{sb})$

$$\begin{aligned}
 \dot{T}T^{-1} &= \begin{bmatrix} \dot{R} & \dot{p} \\ \mathbf{0} & 0 \end{bmatrix} \begin{bmatrix} R^T & -R^T p \\ \mathbf{0} & 1 \end{bmatrix} \\
 &= \begin{bmatrix} \dot{R}R^T & \dot{p} - \dot{R}R^T p \\ \mathbf{0} & 0 \end{bmatrix} \\
 &= \begin{bmatrix} [\omega_s] & v_s \\ \mathbf{0} & 0 \end{bmatrix} \xrightarrow{\substack{v_s \in \mathbb{R}^3 \\ [\omega_s] \in so(3)}} \dot{T}T^{-1} = [\mathcal{V}_s] = \begin{bmatrix} [\omega_s] & v_s \\ \mathbf{0} & 0 \end{bmatrix} \in se(3)
 \end{aligned}$$

$$\mathcal{V}_s = \begin{bmatrix} \omega_s \\ v_s \end{bmatrix} \in \mathbb{R}^6$$

\mathcal{V}_s is defined as **Spatial Twist**
(or spatial velocity in the space frame)

- $[\mathcal{V}_s] \in se(3)$ is the matrix representations of the **spatial twists** $\mathcal{V}_s \in \mathbb{R}^6$ associated with the rigid-body configuration $T \in SE(3)$.
- \mathcal{V}_s does not depend on the choice of the body frame $\{b\}$.

Adjoint Map

~~$$\mathbf{v}_s = \mathbf{T}_{sb} \mathbf{v}_b$$

\downarrow
 4×4

\downarrow
 6×6~~

$$\begin{aligned}
 [\mathbf{v}_b] &= \mathbf{T}^{-1} \dot{\mathbf{T}} \\
 [\mathbf{v}_s] &= \dot{\mathbf{T}} \mathbf{T}^{-1} \quad \longrightarrow \quad [\mathbf{v}_s] = \mathbf{T} [\mathbf{v}_b] \mathbf{T}^{-1} \quad \longrightarrow
 \end{aligned}$$

$$[\mathbf{v}_s] = \begin{bmatrix} \mathbf{R}[\boldsymbol{\omega}_b] \mathbf{R}^T & -\mathbf{R}[\boldsymbol{\omega}_b] \mathbf{R}^T \mathbf{p} + \mathbf{R} \mathbf{v}_b \\ \mathbf{0} & \mathbf{0} \end{bmatrix} \xrightarrow[\substack{[\boldsymbol{\omega}] \mathbf{p} = -[\mathbf{p}] \boldsymbol{\omega} \\ \mathbf{p}, \boldsymbol{\omega} \in \mathbb{R}^3}]{\mathbf{R}[\boldsymbol{\omega}] \mathbf{R}^T = [\mathbf{R} \boldsymbol{\omega}]} = \begin{bmatrix} [\mathbf{R} \boldsymbol{\omega}_b] & [\mathbf{p}] \mathbf{R} \boldsymbol{\omega}_b + \mathbf{R} \mathbf{v}_b \\ \mathbf{0} & \mathbf{0} \end{bmatrix}$$

$$\Rightarrow \mathbf{v}_s = \begin{bmatrix} \boldsymbol{\omega}_s \\ \mathbf{v}_s \end{bmatrix} = \begin{bmatrix} \mathbf{R} \boldsymbol{\omega}_b \\ [\mathbf{p}] \mathbf{R} \boldsymbol{\omega}_b + \mathbf{R} \mathbf{v}_b \end{bmatrix} = \begin{bmatrix} \mathbf{R} & \mathbf{0} \\ [\mathbf{p}] \mathbf{R} & \mathbf{R} \end{bmatrix} \begin{bmatrix} \boldsymbol{\omega}_b \\ \mathbf{v}_b \end{bmatrix} = [\text{Ad}_T] \mathbf{v}_b$$

$$[\text{Ad}_T] = \begin{bmatrix} \mathbf{R} & \mathbf{0} \\ [\mathbf{p}] \mathbf{R} & \mathbf{R} \end{bmatrix} \in \mathbb{R}^{6 \times 6} \quad \text{Adjoint Map associated with } \mathbf{T} \text{ or Adjoint Representation of } \mathbf{T}$$

• Therefore, $\mathbf{v}_s = [\text{Ad}_{T_{sb}}] \mathbf{v}_b = \text{Ad}_{T_{sb}}(\mathbf{v}_b)$

Similarly, $\mathbf{v}_b = [\text{Ad}_{T_{bs}}] \mathbf{v}_s = \text{Ad}_{T_{bs}}(\mathbf{v}_s)$

Adjoint Map Properties

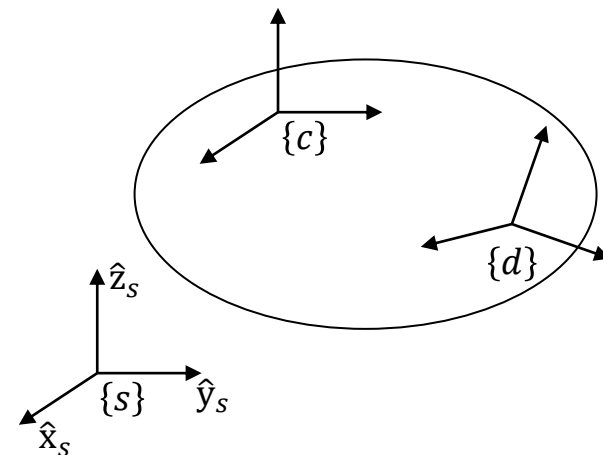
- Let $T_1, T_2 \in SE(3)$ and $\mathcal{V} = (\boldsymbol{\omega}, \boldsymbol{v}) \in \mathbb{R}^6$. Then,

$$[\text{Ad}_{T_1}][\text{Ad}_{T_2}]\mathcal{V} = [\text{Ad}_{T_1 T_2}]\mathcal{V} \quad \text{or} \quad \text{Ad}_{T_1}(\text{Ad}_{T_2}(\mathcal{V})) = \text{Ad}_{T_1 T_2}(\mathcal{V})$$

- For any $T \in SE(3)$, $[\text{Ad}_T]^{-1} = [\text{Ad}_{T^{-1}}]$. Note that $[\text{Ad}_T]$ is always invertible.
- For any two frames $\{c\}$ and $\{d\}$, a twist represented in $\{c\}$ as \mathcal{V}_c is related to its representation in $\{d\}$ as \mathcal{V}_d by

$$\mathcal{V}_c = [\text{Ad}_{T_{cd}}]\mathcal{V}_d \quad \mathcal{V}_d = [\text{Ad}_{T_{dc}}]\mathcal{V}_c$$

(changing the reference frame of a twist)

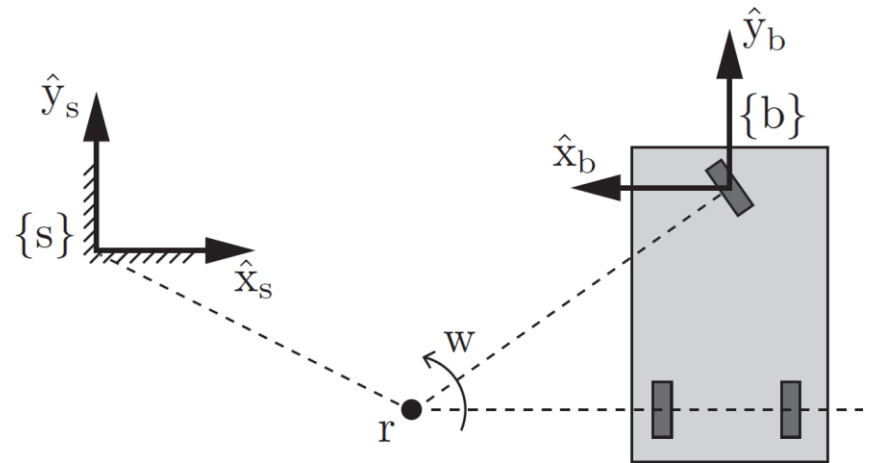


Example

Consider a three-wheeled car with a single steerable front wheel, driving on a plane. The angle of the front wheel of the car causes the car's motion to be a pure angular velocity 2 rad/s about an axis out of the page at the point r in the plane. Find \mathcal{V}_s and \mathcal{V}_b .

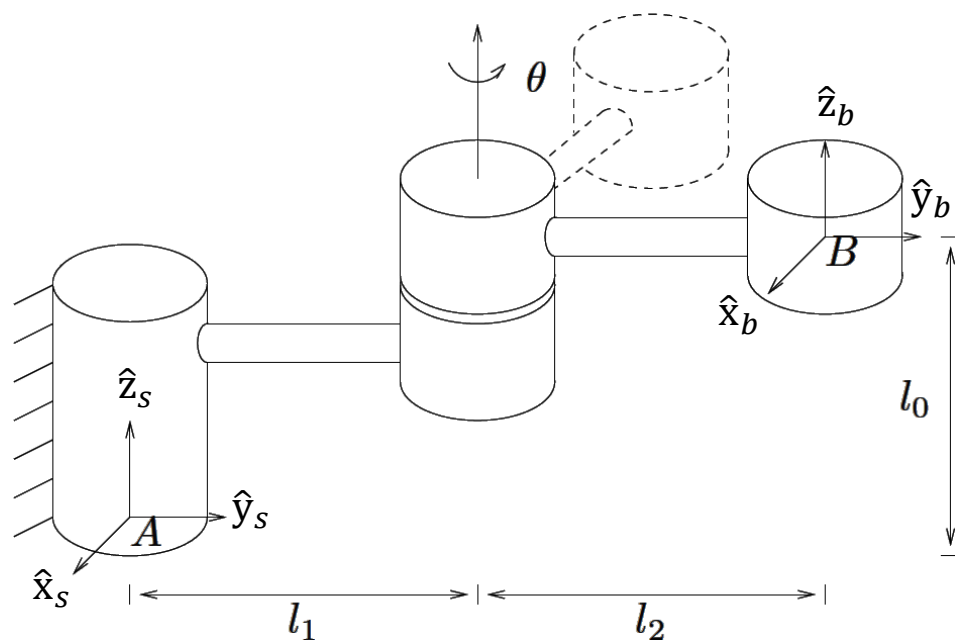
$$\mathbf{r}_s = (2, -1, 0)$$

$$\mathbf{r}_b = (2, -1.4, 0)$$



Example

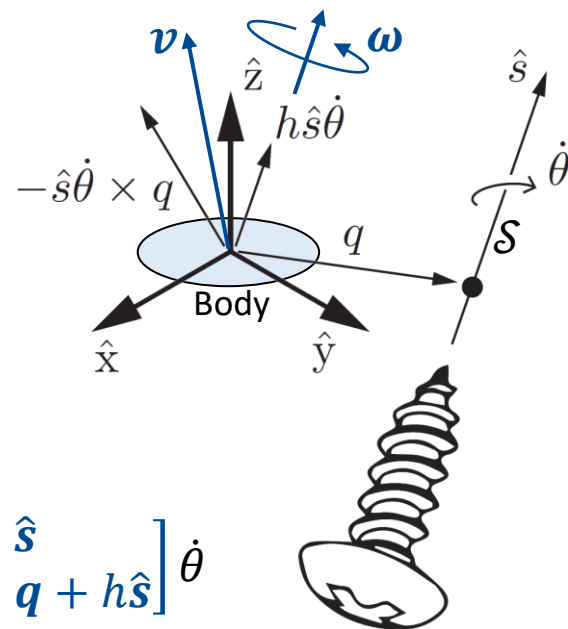
Find \mathcal{V}_s and \mathcal{V}_b for the shown one degree of freedom manipulator.



Screw Interpretation of a Twist

Any rigid-body velocity or twist \mathcal{V} is equivalent to the instantaneous velocity $\dot{\theta}$ about some screw axis \mathcal{S} (i.e., rotating about the axis while also translating along the axis).

A screw axis \mathcal{S} represented by a point $\mathbf{q} \in \mathbb{R}^3$ on the axis, a unit vector $\hat{\mathbf{s}} \in S^2$ in the direction of the axis, and a pitch $h_+ \in \mathbb{R}$ (which is linear velocity along the axis divided by angular velocity $\dot{\theta}$ about the axis) as $\{\mathbf{q}, \hat{\mathbf{s}}, h\}$.



Thus, twist \mathcal{V} can be represented as

$$\mathcal{V} = \begin{bmatrix} \boldsymbol{\omega} \\ \mathbf{v} \end{bmatrix} = \begin{bmatrix} \boldsymbol{\omega} \\ \boldsymbol{\omega} \times (-\mathbf{q}) + h\boldsymbol{\omega} \end{bmatrix} = \begin{bmatrix} \hat{\mathbf{s}}\dot{\theta} \\ -\hat{\mathbf{s}}\dot{\theta} \times \mathbf{q} + h\dot{\theta}\hat{\mathbf{s}} \end{bmatrix} = \begin{bmatrix} \hat{\mathbf{s}} \\ -\hat{\mathbf{s}} \times \mathbf{q} + h\hat{\mathbf{s}} \end{bmatrix} \dot{\theta}$$

Due to rotation about \mathcal{S}
(which is in the plane orthogonal to $\hat{\mathbf{s}}$)

Due to translation along \mathcal{S}
(which is in the direction of $\hat{\mathbf{s}}$)

Representation of Screw Axis

Now, instead of representing the screw axis \mathcal{S} as $\{\mathbf{q}, \hat{\mathbf{s}}, h\}$ (where \mathbf{q} is not unique), we represent a “unit” screw axis (uniquely) as a vector as

$$\mathbf{s} = \begin{bmatrix} \mathbf{S}_\omega \\ \mathbf{S}_v \end{bmatrix} \in \mathbb{R}^6 \quad \text{where} \quad \mathbf{v} = \mathbf{s}\dot{\theta} \in \mathbb{R}^6 \quad \mathbf{S}_\omega, \mathbf{S}_v \in \mathbb{R}^3$$

• Finding \mathbf{S} and $\{\mathbf{q}, \hat{\mathbf{s}}, h\}$ by having \mathbf{v} :

(a) If $\|\boldsymbol{\omega}\| \neq 0$ (\equiv rotation with/without translation along $\hat{\mathbf{s}}$):

$$\begin{aligned} \mathbf{S} = \begin{bmatrix} \mathbf{S}_\omega \\ \mathbf{S}_v \end{bmatrix} &= \mathbf{v} / \|\boldsymbol{\omega}\| = \begin{bmatrix} \boldsymbol{\omega} / \|\boldsymbol{\omega}\| \\ \mathbf{v} / \|\boldsymbol{\omega}\| \end{bmatrix} = \begin{bmatrix} \hat{\mathbf{s}} \\ -\hat{\mathbf{s}} \times \mathbf{q} + h\hat{\mathbf{s}} \end{bmatrix} \\ &= \begin{bmatrix} \text{angular velocity when } \dot{\theta} = 1 \\ \text{linear velocity of origin when } \dot{\theta} = 1 \end{bmatrix} \end{aligned}$$

Pitch h is finite ($h = 0$ for pure rotation).
 $h = \mathbf{S}_\omega^T \mathbf{S}_v = \boldsymbol{\omega}^T \mathbf{v} / \|\boldsymbol{\omega}\|^2$
 $\hat{\mathbf{s}} = \mathbf{S}_\omega = \boldsymbol{\omega} / \|\boldsymbol{\omega}\|, \quad \|\mathbf{S}_\omega\| = 1$
 $\dot{\theta} = \|\boldsymbol{\omega}\|$ is interpreted as angular velocity about $\hat{\mathbf{s}}$
 To find \mathbf{q} , use $\mathbf{v} - h\boldsymbol{\omega} = -\boldsymbol{\omega} \times \mathbf{q}$
 or $(\mathbf{S}_v - h\mathbf{S}_\omega = -\mathbf{S}_\omega \times \mathbf{q})$

(b) If $\|\boldsymbol{\omega}\| = 0$ (\equiv pure translation along $\hat{\mathbf{s}}$):

$$\begin{aligned} \mathbf{S} = \begin{bmatrix} \mathbf{S}_\omega \\ \mathbf{S}_v \end{bmatrix} &= \mathbf{v} / \|\mathbf{v}\| = \begin{bmatrix} \mathbf{0} \\ \mathbf{v} / \|\mathbf{v}\| \end{bmatrix} = \begin{bmatrix} \mathbf{0} \\ \hat{\mathbf{s}} \end{bmatrix} \\ &= \begin{bmatrix} \mathbf{0} \\ \text{normalized linear velocity of origin} \end{bmatrix} \end{aligned}$$

Pitch h is infinite, $\|\mathbf{S}_\omega\| = 0$
 $\hat{\mathbf{s}} = \mathbf{S}_v = \mathbf{v} / \|\mathbf{v}\|, \quad \|\mathbf{S}_v\| = 1$
 $\dot{\theta} = \|\mathbf{v}\|$ is interpreted as linear velocity along $\hat{\mathbf{s}}$

Screw Axis Properties

- ❖ Since a screw axis \mathcal{S} is just a normalized twist, the 4×4 matrix representation $[\mathcal{S}]$ of $\mathcal{S} = (\mathcal{S}_\omega, \mathcal{S}_v) \in \mathbb{R}^6$ is

$$[\mathcal{S}] = \begin{bmatrix} [\mathcal{S}_\omega] & \mathcal{S}_v \\ \mathbf{0} & 0 \end{bmatrix} \in se(3)$$

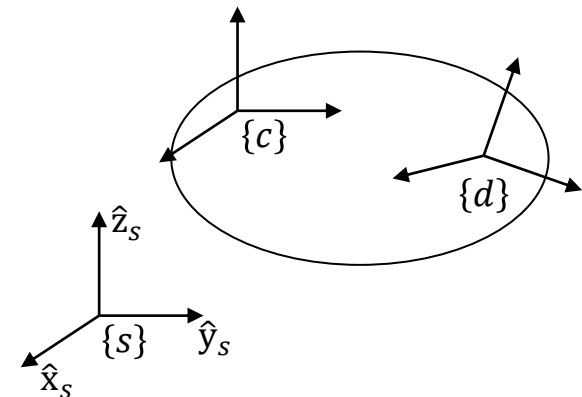
$$\mathcal{V} = \mathcal{S}\dot{\theta} \in \mathbb{R}^6 \quad \Rightarrow \quad [\mathcal{V}] = [\mathcal{S}]\dot{\theta} \in se(3)$$

- ❖ Like twist \mathcal{V} , the screw axis \mathcal{S} is represented in a frame (e.g., $\{b\}$ or $\{s\}$). Therefore, for any two frames $\{c\}$ and $\{d\}$, a screw axis represented in $\{c\}$ as \mathcal{S}_c is related to its representation in $\{d\}$ as \mathcal{S}_d by:

$$\mathcal{S}_c = [\text{Ad}_{T_{cd}}] \mathcal{S}_d$$

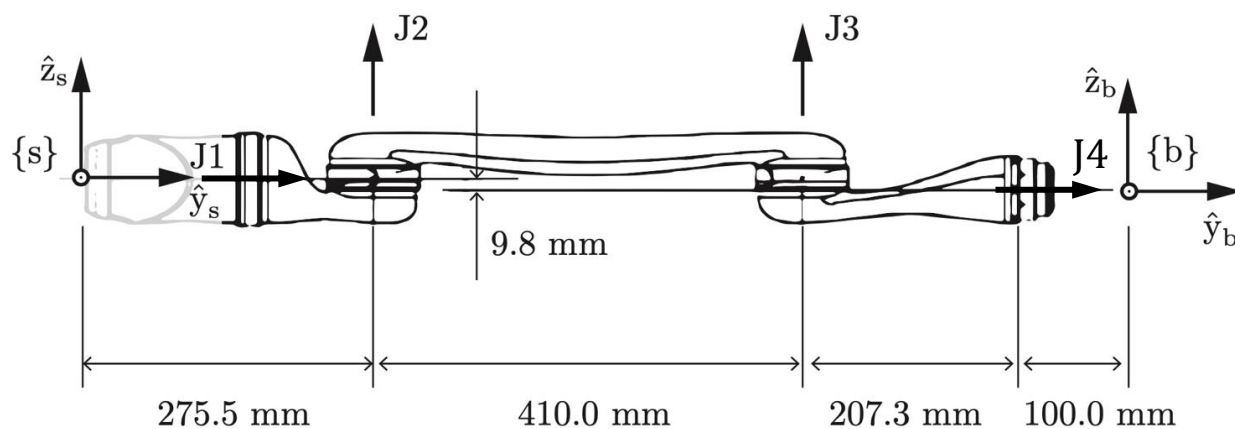
$$\mathcal{S}_d = [\text{Ad}_{T_{dc}}] \mathcal{S}_c$$

(changing the reference frame of a screw axis)



Example

What are the screw axis \mathcal{S}_b and \mathcal{S}_s for J4 and J2 for the shown Kinova 4-DOF arm?



Exponential Coordinate Representation of Rigid-Body Motion

Screw Motion

Instead of viewing a displacement as a rotation followed by a translation, both rotation and translation can be performed simultaneously.

Planar example of a screw motion:

The displacement in Figure 1 (rotation ① + translation ②) can be viewed as a pure rotation of $\beta = 90^\circ$ about a fixed-point s as shown in Figure 2.

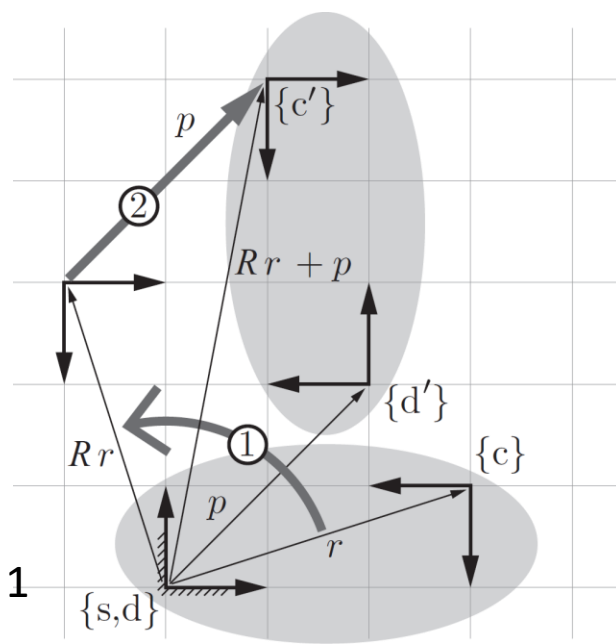


Figure 1

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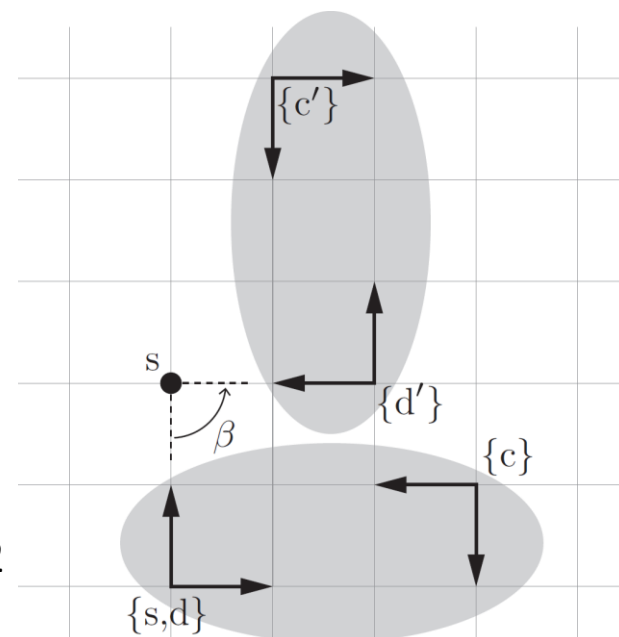


Figure 2

Exponential Coordinates of Rigid-Body Motions

Chasles–Mozzi theorem states that every rigid-body displacement can be expressed as a finite rotation and translation about a fixed screw axis in space.

This theorem motivates a six-parameter representation of a configuration (or a homogeneous transformation $\mathbf{T} \in SE(3)$) called the **exponential coordinates** as $\mathbf{S}\theta \in \mathbb{R}^6$, where \mathbf{S} is the screw axis and θ is the distance that must be traveled along the screw axis to take a frame from the origin \mathbf{I}_4 to \mathbf{T} .

Note: \mathbf{T} is equivalent to the displacement obtained by rotating a frame from \mathbf{I}_3 about \mathbf{S}

- by an angle θ , or
- at a speed $\dot{\theta} = 1$ rad/s for θ s, or
- at a speed $\dot{\theta} = \theta$ for 1s, or
- by constant twist \mathcal{V} for 1s.

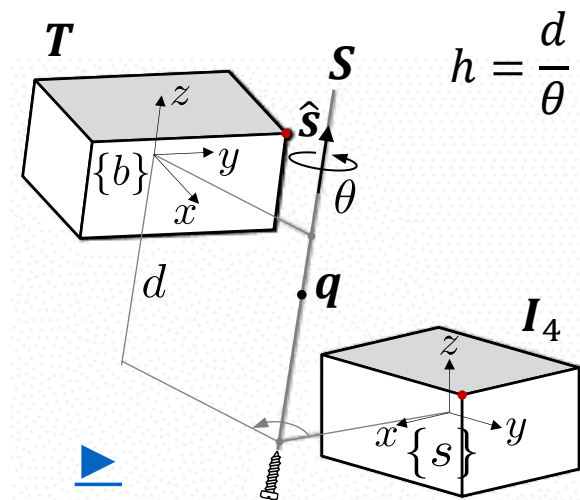
$$(\mathcal{V}t = \mathbf{S}\theta)$$

Constant Screw Motion:

A rotation θ + a translation d about/along a fixed screw axis \mathbf{S} .

$$\mathbf{S} = \begin{bmatrix} \mathbf{S}_\omega \\ \mathbf{S}_v \end{bmatrix} = \begin{bmatrix} \hat{\mathbf{s}} \\ -\hat{\mathbf{s}} \times \mathbf{q} + h\hat{\mathbf{s}} \end{bmatrix} \quad (\text{for rotation with/without translation along } \hat{\mathbf{s}})$$

$$\mathbf{S} = \begin{bmatrix} \mathbf{S}_\omega \\ \mathbf{S}_v \end{bmatrix} = \begin{bmatrix} \mathbf{0} \\ \hat{\mathbf{s}} \end{bmatrix} \quad (\text{for pure translation along } \hat{\mathbf{s}})$$



Exponential Coordinates of Rigid-Body Motions

As with rotations, we can define a matrix exponential (exp) and matrix logarithm (log).

For any transformation matrix $\mathbf{T} \in SE(3)$, we can always find a screw axis $\mathbf{S} = (\mathbf{S}_\omega, \mathbf{S}_v) \in \mathbb{R}^6$ ($\|\mathbf{S}_\omega\| = 1$ or $\mathbf{S}_\omega = \mathbf{0}$, $\|\mathbf{S}_v\| = 1$) and scalar $\theta \in \mathbb{R}$ such that $\mathbf{T} = e^{[\mathbf{S}]\theta}$.

$$\text{exp: } [\mathbf{S}]\theta \in se(3) \rightarrow \mathbf{T} \in SE(3) \quad : \quad e^{[\mathbf{S}]\theta} = \mathbf{T} = (\mathbf{R}, \mathbf{p})$$

$$\text{log: } \mathbf{T} \in SE(3) \rightarrow [\mathbf{S}]\theta \in se(3) \quad : \quad \log(\mathbf{T}) = [\mathbf{S}]\theta$$

$\mathbf{S}\theta \in \mathbb{R}^6$: Exponential coordinates of $\mathbf{T} \in SE(3)$

$[\mathbf{S}]\theta = [\mathbf{S}\theta] \in se(3)$: Matrix logarithm of \mathbf{T} (inverse of the matrix exponential)

Note: \mathbf{T} and \mathbf{S} have the same base.

Matrix Exponential

$$\text{exp: } [\mathbf{S}]\theta \in se(3) \rightarrow \mathbf{T} \in SE(3) \quad : \quad e^{[\mathbf{S}]\theta} = \mathbf{T} = (\mathbf{R}, \mathbf{p})$$

❖ Finding $\mathbf{T} = (\mathbf{R}, \mathbf{p})$ by having $\mathbf{S} = (\mathbf{S}_\omega, \mathbf{S}_v)$ and θ :

$$e^{[\mathbf{S}]\theta} = \begin{bmatrix} e^{[\mathbf{S}_\omega]\theta} & \mathbf{G}(\theta)\mathbf{S}_v \\ \mathbf{0} & 1 \end{bmatrix} = \begin{bmatrix} \mathbf{R} & \mathbf{p} \\ \mathbf{0} & 1 \end{bmatrix}$$

Using Taylor expansion

Use Rodrigues Formula

$$\mathbf{G}(\theta) = \mathbf{I}_3\theta + (1 - \cos \theta)[\mathbf{S}_\omega] + (\theta - \sin \theta)[\mathbf{S}_\omega]^2 \in \mathbb{R}^{3 \times 3}$$

Matrix Exponential: Remark

- For a given transformation matrix T_{sb} :

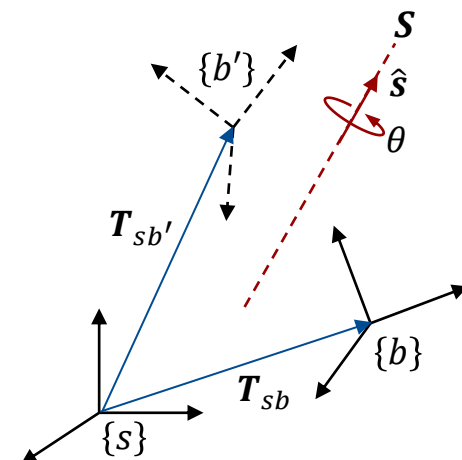
Fixed-frame Displacement is rotation by θ about/along a screw axis S_s , expressed in fixed frame $\{s\}$ as:

$$T_{sb'} = e^{[S_s]\theta} T_{sb}$$

Body-frame Displacement is rotation by θ about/along a screw axis S_b , expressed in body frame $\{b\}$ as:

$$T_{sb'} = T_{sb} e^{[S_b]\theta}$$

$$(S_s = [Ad_{T_{sb}}]S_b)$$



Matrix Logarithm

$$\log: \quad \mathbf{T} \in SE(3) \quad \rightarrow \quad [\mathbf{S}]\theta \in se(3) \quad : \quad \log(\mathbf{T}) = [\mathbf{S}]\theta$$

❖ Finding $\mathbf{S} = (\mathbf{S}_\omega, \mathbf{S}_v)$ and $\theta \in [0, \pi]$ by having $\mathbf{T} = (\mathbf{R}, \mathbf{p})$:

(a) If $\text{tr}\mathbf{R} = 3$ (or $\mathbf{R} = \mathbf{I}_3$), then set $\mathbf{S}_\omega = \mathbf{0}$, $\mathbf{S}_v = \mathbf{p}/\|\mathbf{p}\|$, and $\theta = \|\mathbf{p}\|$.

(b) Otherwise, use the matrix logarithm $\log(\mathbf{R}) = [\mathbf{S}_\omega]\theta$ to determine \mathbf{S}_ω ($\hat{\boldsymbol{\omega}}$ in the $SO(3)$ algorithm) and $\theta \in [0, \pi]$. Then, \mathbf{S}_v is calculated as

$$\mathbf{S}_v = \mathbf{G}^{-1}(\theta)\mathbf{p}$$

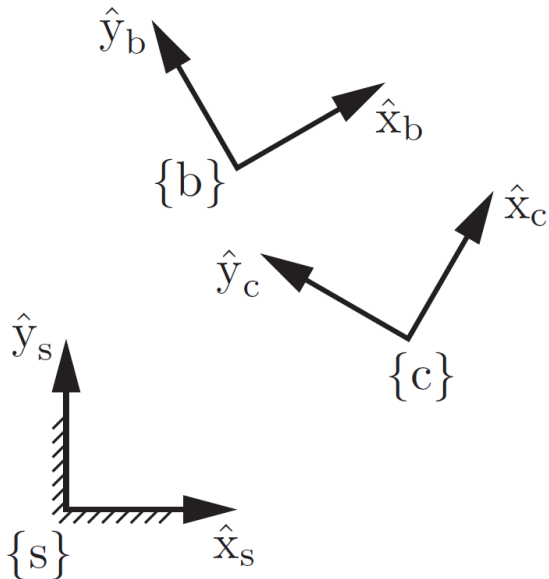
$$\text{where } \mathbf{G}^{-1}(\theta) = \frac{1}{\theta}\mathbf{I}_3 - \frac{1}{2}[\mathbf{S}_\omega] + \left(\frac{1}{\theta} - \frac{1}{2}\cot\frac{\theta}{2}\right)[\mathbf{S}_\omega]^2 \in \mathbb{R}^{3 \times 3}$$

Example

The initial frame $\{b\}$ and final frame $\{c\}$ are given. Find the screw motion expressed in $\{s\}$ (\mathcal{S}_s, θ) that displaces the frame at T_{sb} to T_{sc} .

$$T_{sb} = \begin{bmatrix} \cos 30^\circ & -\sin 30^\circ & 0 & 1 \\ \sin 30^\circ & \cos 30^\circ & 0 & 2 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_{sc} = \begin{bmatrix} \cos 60^\circ & -\sin 60^\circ & 0 & 2 \\ \sin 60^\circ & \cos 60^\circ & 0 & 1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



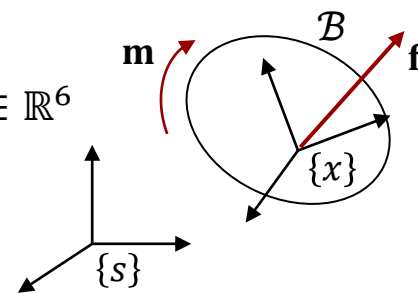
Wrench

Spatial Force or Wrench

A rigid body's **Spatial Force** or **Wrench** can be represented as a point in \mathbb{R}^6 and defined as

expressed in $\{x\}$

$$\mathcal{F}_x = \begin{bmatrix} \text{moment applied to body expressed in frame } \{x\} \\ \text{force applied to origin of frame } \{x\} \text{ on body expressed in frame } \{x\} \end{bmatrix} \in \mathbb{R}^6$$

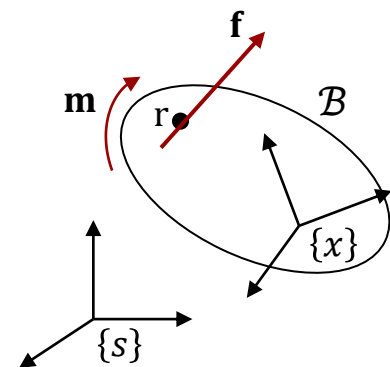


A general form:

point where force is applied

$$\mathcal{F}_x^{B_r} = \begin{bmatrix} \text{moment applied to body } \mathcal{B} + \text{moment of force applied to point } r \text{ on body } \mathcal{B} \text{ in } \{x\} \\ \text{force applied to point } r \text{ on body } \mathcal{B} \text{ expressed in frame } \{x\} \end{bmatrix} \in \mathbb{R}^6$$

expressed in $\{x\}$



Body Wrench \mathcal{F}_b

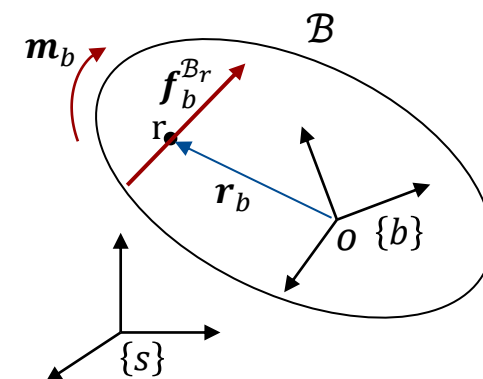
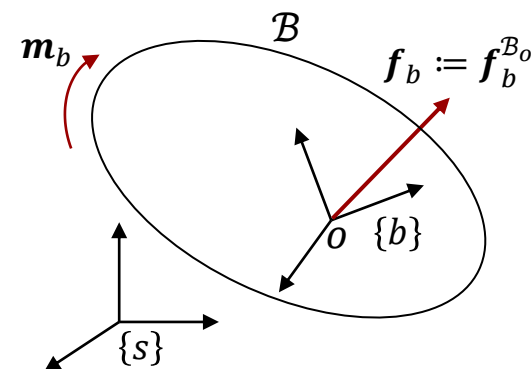
Let $\mathbf{m}_b \in \mathbb{R}^3$ be a moment applied to the body expressed in $\{b\}$ and $\mathbf{f}_b \in \mathbb{R}^3$ be a force applied to the body at the origin of frame $\{b\}$ and expressed in $\{b\}$. **Body Wrench \mathcal{F}_b** is defined as

$$\mathcal{F}_b = \begin{bmatrix} \mathbf{m}_b \\ \mathbf{f}_b \end{bmatrix} \in \mathbb{R}^6$$

General Case: If force \mathbf{f} is applied at the point r of body \mathcal{B} , the body wrench in $\{b\}$ will be:

$$\mathcal{F}_b^{\mathcal{B}r} = \begin{bmatrix} \mathbf{m}_b + \mathbf{r}_b \times \mathbf{f}_b^{\mathcal{B}r} \\ \mathbf{f}_b^{\mathcal{B}r} \end{bmatrix} \in \mathbb{R}^6$$

where $\mathbf{r}_b \in \mathbb{R}^3$ is the position vector of point r in $\{b\}$ and $\mathbf{r}_b \times \mathbf{f}_b^{\mathcal{B}r}$ is the moment created by force $\mathbf{f}_b^{\mathcal{B}r}$ about the origin of $\{b\}$.



Spatial Wrench \mathcal{F}_s

The **power** is a coordinate-independent quantity, i.e., the power generated (or dissipated) by a wrench \mathcal{F} and twist \mathcal{V} pair must be the same regardless of the frame in which it is represented:

$$(\mathcal{V} \cdot \mathcal{F} = \text{power}) \quad \mathcal{V}_s^T \mathcal{F}_s = \mathcal{V}_b^T \mathcal{F}_b = \text{power} \quad (\mathcal{V}_b = [\text{Ad}_{T_{bs}}] \mathcal{V}_s)$$

$$\begin{aligned} \mathcal{V}_s^T \mathcal{F}_s &= ([\text{Ad}_{T_{bs}}] \mathcal{V}_s)^T \mathcal{F}_b \\ &= \mathcal{V}_s^T [\text{Ad}_{T_{bs}}]^T \mathcal{F}_b \end{aligned}$$

Since this must hold for all \mathcal{V}_s

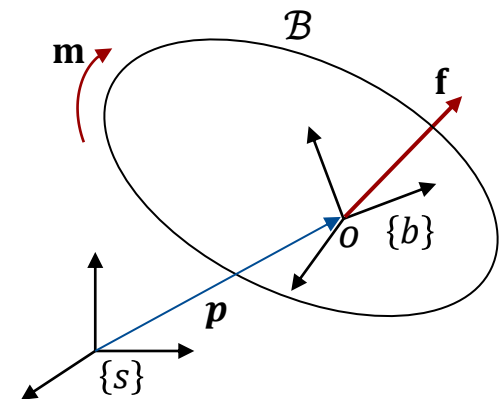
$$\mathcal{F}_s = [\text{Ad}_{T_{bs}}]^T \mathcal{F}_b$$

spatial wrench

body wrench

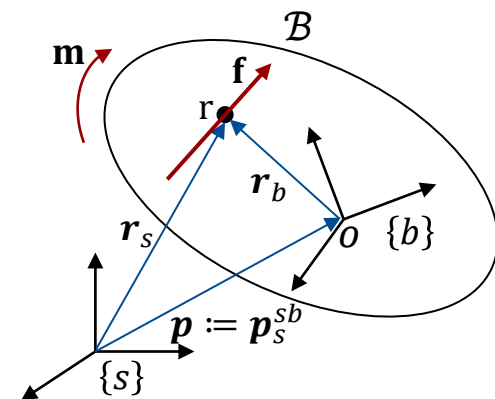
Therefore:

$$\mathcal{F}_s = [\text{Ad}_{T_{bs}}]^T \begin{bmatrix} \mathbf{m}_b \\ \mathbf{f}_b \end{bmatrix} = \begin{bmatrix} \mathbf{m}_s + \mathbf{p} \times \mathbf{f}_s \\ \mathbf{f}_s \end{bmatrix}$$



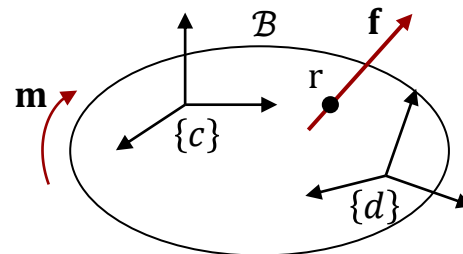
Spatial Wrench \mathcal{F}_s : General Case

$$\begin{aligned} \mathcal{F}_s^{\mathcal{B}_r} &= [\text{Ad}_{T_{bs}}]^T \mathcal{F}_b^{\mathcal{B}_r} = \begin{bmatrix} \mathbf{R}_{sb} & -\mathbf{R}_{sb}[\mathbf{p}_b^{bs}] \\ \mathbf{0} & \mathbf{R}_{sb} \end{bmatrix} \begin{bmatrix} \mathbf{m}_b^{\mathcal{B}} + \mathbf{r}_b \times \mathbf{f}_b^{\mathcal{B}_r} \\ \mathbf{f}_b^{\mathcal{B}_r} \end{bmatrix} = \begin{bmatrix} \mathbf{R}_{sb} \mathbf{m}_b^{\mathcal{B}} + \mathbf{R}_{sb} \left((\mathbf{r}_b - \mathbf{p}_b^{bs}) \times \mathbf{f}_b^{\mathcal{B}_r} \right) \\ \mathbf{R}_{sb} \mathbf{f}_b^{\mathcal{B}_r} \end{bmatrix} \\ &= \begin{bmatrix} \mathbf{R}_{sb} \mathbf{m}_b^{\mathcal{B}} + \mathbf{R}_{sb} \mathbf{p}_b^{sr} \times \mathbf{R}_{sb} \mathbf{f}_b^{\mathcal{B}_r} \\ \mathbf{R}_{sb} \mathbf{f}_b^{\mathcal{B}_r} \end{bmatrix} = \begin{bmatrix} \mathbf{m}_s^{\mathcal{B}} + \mathbf{r}_s \times \mathbf{f}_s^{\mathcal{B}_r} \\ \mathbf{f}_s^{\mathcal{B}_r} \end{bmatrix} \in \mathbb{R}^6 \end{aligned}$$



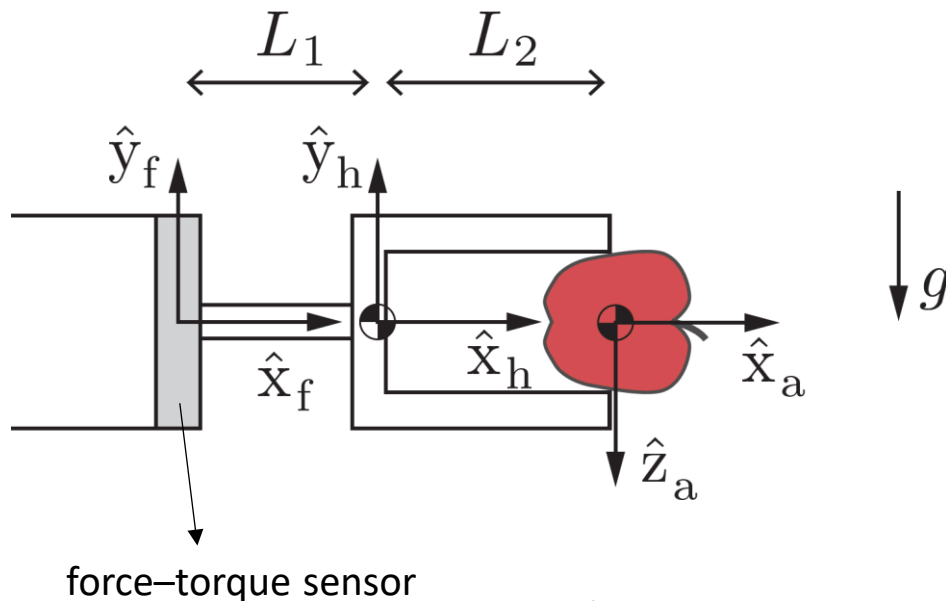
- In general, if we have the wrench in frame $\{d\}$, we can express it in another frame $\{c\}$ as:

$$\mathcal{F}_c^{\mathcal{B}_r} = [\text{Ad}_{T_{dc}}]^T \mathcal{F}_d^{\mathcal{B}_r}$$



Example

The robot hand shown is holding an apple with a mass of 0.1 kg in a gravitational field $g=10 \text{ m/s}^2$. The mass of the hand is 0.5 kg, $L_1=10 \text{ cm}$, and $L_2=15 \text{ cm}$. What is the force and torque measured by the six-axis force–torque sensor between the hand and the robot arm?



- ❖ **Note:** If more than one wrench acts on a rigid body, the total wrench on the body is simply the vector sum of the individual wrenches, provided that the wrenches are expressed in the same frame.

Review

Rigid-Body Motions

Rotations	Rigid-Body Motions
$\mathbf{R} \in SO(3)$: 3×3 matrices $\mathbf{R}^T \mathbf{R} = \mathbf{R} \mathbf{R}^T = \mathbf{I}_3, \det(\mathbf{R}) = 1$	$\mathbf{T} \in SE(3)$: 4×4 matrices $\mathbf{T} = \begin{bmatrix} \mathbf{R} & \mathbf{p} \\ \mathbf{0} & 1 \end{bmatrix},$ where $\mathbf{R} \in SO(3), \mathbf{p} \in \mathbb{R}^3$
$\mathbf{R}^{-1} = \mathbf{R}^T$	$\mathbf{T}^{-1} = \begin{bmatrix} \mathbf{R}^T & -\mathbf{R}^T \mathbf{p} \\ \mathbf{0} & 1 \end{bmatrix}$
Change of coordinate frame: $\mathbf{R}_{ab} \mathbf{R}_{bc} = \mathbf{R}_{ac}, \mathbf{R}_{ab} \mathbf{p}_b = \mathbf{p}_a$ $(\mathbf{R}_{ab} = \mathbf{R}_{ba}^{-1} = \mathbf{R}_{ba}^T)$	Change of coordinate frame: $\mathbf{T}_{ab} \mathbf{T}_{bc} = \mathbf{T}_{ac}, \mathbf{T}_{ab} \mathbf{p}_b = \mathbf{p}_a$ $(\mathbf{T}_{ab} = \mathbf{T}_{ba}^{-1})$

Rigid-Body Motions

Rotations	Rigid-Body Motions
Rotating a frame {b}: $\mathbf{R} = \text{Rot}(\hat{\omega}, \theta)$ $\mathbf{R}_{sb'} = \mathbf{R}\mathbf{R}_{sb}$ rotate θ about $\hat{\omega}_s = \hat{\omega}$ $\mathbf{R}_{sb'} = \mathbf{R}_{sb}\mathbf{R}$ rotate θ about $\hat{\omega}_b = \hat{\omega}$	Displacing a frame {b}: $\mathbf{T} = \begin{bmatrix} \text{Rot}(\hat{\omega}, \theta) & \mathbf{p} \\ \mathbf{0} & 1 \end{bmatrix}$ $\mathbf{T}_{sb'} = \mathbf{T}\mathbf{T}_{sb}$ rotate θ about $\hat{\omega}_s = \hat{\omega}$ (moves {b} origin), translate \mathbf{p} in {s} $\mathbf{T}_{sb'} = \mathbf{T}_{sb}\mathbf{T}$ translate \mathbf{p} in {b}, rotate θ about $\hat{\omega}$ in new body frame
Unit rotation axis is $\hat{\omega} \in \mathbb{R}^3$, where $\ \hat{\omega}\ = 1$	“Unit” screw axis is $\mathbf{S} = \begin{bmatrix} \mathbf{S}_\omega \\ \mathbf{S}_v \end{bmatrix} \in \mathbb{R}^6$, where either (i) $\ \mathbf{S}_\omega\ = 1$ or (ii) $\ \mathbf{S}_\omega\ = 0, \ \mathbf{S}_v\ = 1$
	For a screw axis $\{\mathbf{q}, \hat{\mathbf{s}}, h\}$ with finite h , $\mathbf{S} = \begin{bmatrix} \mathbf{S}_\omega \\ \mathbf{S}_v \end{bmatrix} = \begin{bmatrix} \hat{\mathbf{s}} \\ -\hat{\mathbf{s}} \times \mathbf{q} + h\hat{\mathbf{s}} \end{bmatrix}$
Angular velocity is $\boldsymbol{\omega} = \hat{\omega}\dot{\theta}$	Twist is $\boldsymbol{\mathcal{V}} = \mathbf{S}\dot{\theta}$

Rigid-Body Motions

Rotations	Rigid-Body Motions
<p>For any $\boldsymbol{\omega} = (\omega_1, \omega_2, \omega_3) \in \mathbb{R}^3$,</p> $[\boldsymbol{\omega}] = \begin{bmatrix} 0 & -\omega_3 & \omega_2 \\ \omega_3 & 0 & -\omega_1 \\ -\omega_2 & \omega_1 & 0 \end{bmatrix} \in so(3)$ <p>Properties: For any $\boldsymbol{\omega}, \boldsymbol{x} \in \mathbb{R}^3, \boldsymbol{R} \in SO(3)$:</p> $[\boldsymbol{\omega}] = -[\boldsymbol{\omega}]^T, [\boldsymbol{\omega}]\boldsymbol{x} = -[\boldsymbol{x}]\boldsymbol{\omega},$ $[\boldsymbol{\omega}][\boldsymbol{x}] = ([\boldsymbol{x}][\boldsymbol{\omega}])^T, \boldsymbol{R}[\boldsymbol{\omega}]\boldsymbol{R}^T = [\boldsymbol{R}\boldsymbol{\omega}]$	<p>For any $\boldsymbol{v} = \begin{bmatrix} \boldsymbol{\omega} \\ \boldsymbol{v} \end{bmatrix} \in \mathbb{R}^6$ or $\boldsymbol{S} = \begin{bmatrix} \boldsymbol{S}_\omega \\ \boldsymbol{S}_v \end{bmatrix} \in \mathbb{R}^6$,</p> $[\boldsymbol{v}] = \begin{bmatrix} [\boldsymbol{\omega}] & \boldsymbol{v} \\ \mathbf{0} & 0 \end{bmatrix} \in se(3),$ $[\boldsymbol{S}] = \begin{bmatrix} [\boldsymbol{S}_\omega] & \boldsymbol{S}_v \\ \mathbf{0} & 0 \end{bmatrix} \in se(3)$
$\dot{\boldsymbol{R}}\boldsymbol{R}^{-1} = [\boldsymbol{\omega}_s], \quad \boldsymbol{R}^{-1}\dot{\boldsymbol{R}} = [\boldsymbol{\omega}_b] \quad (\boldsymbol{R} := \boldsymbol{R}_{sb})$	$\dot{\boldsymbol{T}}\boldsymbol{T}^{-1} = [\boldsymbol{v}_s], \quad \boldsymbol{T}^{-1}\dot{\boldsymbol{T}} = [\boldsymbol{v}_b] \quad (\boldsymbol{T} := \boldsymbol{T}_{sb})$
	$[\text{Ad}_{\boldsymbol{T}}] = \begin{bmatrix} \boldsymbol{R} & \mathbf{0} \\ [\boldsymbol{p}]\boldsymbol{R} & \boldsymbol{R} \end{bmatrix} \in \mathbb{R}^{6 \times 6}$ <p>Properties: $[\text{Ad}_{\boldsymbol{T}}]^{-1} = [\text{Ad}_{\boldsymbol{T}^{-1}}]$,</p> $[\text{Ad}_{\boldsymbol{T}_1}][\text{Ad}_{\boldsymbol{T}_2}] = [\text{Ad}_{\boldsymbol{T}_1\boldsymbol{T}_2}]$
<p>Change of coordinate frame:</p> $\hat{\boldsymbol{\omega}}_a = \boldsymbol{R}_{ab}\hat{\boldsymbol{\omega}}_b, \quad \boldsymbol{\omega}_a = \boldsymbol{R}_{ab}\boldsymbol{\omega}_b$	<p>Change of coordinate frame:</p> $\boldsymbol{S}_a = [\text{Ad}_{\boldsymbol{T}_{ab}}]\boldsymbol{S}_b, \quad \boldsymbol{v}_a = [\text{Ad}_{\boldsymbol{T}_{ab}}]\boldsymbol{v}_b$

Rigid-Body Motions

Rotations	Rigid-Body Motions
$\hat{\omega}_s = \mathbf{R}_{sb} \hat{\omega}_b$	$\mathbf{S}_s = [\text{Ad}_{T_{sb}}] \mathbf{S}_b, \mathbf{V}_s = [\text{Ad}_{T_{sb}}] \mathbf{V}_b, [\text{Ad}_T] = \begin{bmatrix} \mathbf{R} & \mathbf{0} \\ [p] \mathbf{R} & \mathbf{R} \end{bmatrix}$
Exponential coordinate for $\mathbf{R} \in SO(3)$: $\hat{\omega} \theta \in \mathbb{R}^3$	Exponential coordinate for $\mathbf{T} \in SE(3)$: $\mathbf{S} \theta \in \mathbb{R}^6$
exp: $[\hat{\omega}] \theta \in so(3) \rightarrow \mathbf{R} \in SO(3)$ $\mathbf{R} = \text{Rot}(\hat{\omega}, \theta) = e^{[\hat{\omega}] \theta}$ $\mathbf{R} = \mathbf{I}_3 + \sin \theta [\hat{\omega}] + (1 - \cos \theta) [\hat{\omega}]^2$ (Rodrigues' formula for rotations)	exp: $[\mathbf{S}] \theta \in se(3) \rightarrow \mathbf{T} \in SE(3)$ $\mathbf{T} = e^{[\mathbf{S}] \theta}$ $\mathbf{T} = \begin{bmatrix} e^{[\mathbf{S}_\omega] \theta} & \mathbf{G}(\theta) \mathbf{S}_v \\ \mathbf{0} & 1 \end{bmatrix}$ $\mathbf{G}(\theta) = \mathbf{I}_3 \theta + (1 - \cos \theta) [\mathbf{S}_\omega] + (\theta - \sin \theta) [\mathbf{S}_\omega]^2$
log: $\mathbf{R} \in SO(3) \rightarrow [\hat{\omega}] \theta \in so(3)$ $\log(\mathbf{R}) = [\hat{\omega}] \theta$	log: $\mathbf{T} \in SE(3) \rightarrow [\mathbf{S}] \theta \in se(3)$ $\log(\mathbf{T}) = [\mathbf{S}] \theta$
Moment change of coordinate frame: $\mathbf{m}_a = \mathbf{R}_{ab} \mathbf{m}_b$	Wrench change of coordinate frame: $\mathcal{F}_a = (\mathbf{m}_a, \mathbf{f}_a) = [\text{Ad}_{T_{ba}}]^T \mathcal{F}_b$